Characterisation of the normal right ventricular pressure-volume relation by biplane angiography and simultaneous micromanometer pressure measurements

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SUMMARY The normal right ventricular pressure-volume relation was studied by recording biplane right ventriculograms with simultaneous high fidelity pressure recordings in 10 adults found to have normal coronary arteries and haemodynamic function at diagnostic cardiac catheterisation. Right ventricular volume was measured frame by frame from digitised ventriculograms by a modification of Simpson's rule. The accuracy of this method was tested in a study of 22 human and animal right ventricular casts. There was excellent agreement between calculated volumes and those measured by fluid displacement. The derived regression equations were used to correct right ventricular volumes calculated from in vivo studies. The mean (SD) end diastolic volume index for the group was 62 (13) ml/m², the stroke volume index was 43 (8) ml/m², and the ejection fraction was 62 (6)%. Right ventricular pressure-volume loops were generated by combining simultaneous volume and pressure curves. The normal right ventricular pressure-volume loop was triangular, departing significantly from the square or rectangle of the normal left ventricular pressure-volume loop. Ejection from the right ventricle began early during the pressure rise and continued as right ventricular pressure fell. As a result phases of isovolumic contraction and relaxation were difficult to define.

These observations show that normal right ventricular pressure-volume relations differ considerably from those of the normal left ventricle, presumably reflecting the different loading conditions of the two ventricles.

Unlike the left ventricle, the right ventricle has been largely ignored in terms of the detailed characterisation of its function. Probably the most important factor responsible for this has been the difficulty in accurately measuring right ventricular volume as a result of its complex geometric shape. Unlike the normal left ventricle, which approximates to a prolate ellipsoid, the right ventricle does not lend itself to volume calculation on the basis of a simple geometric assumption. None the less, various methods

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have been used, including simple area-length algorithms and geometric models¹⁻³ and the use of Simpson's rule, which permits the measurement of the volume of a complex shape by dividing it into a series of slices.^{2 4 5} Although they require computer techniques to make such measurements practicable, methods incorporating Simpson's rule can be applied to the determination of right ventricular volume both throughout the cardiac cycle and as it is affected by disease.

Although the importance of right ventricular dysfunction in the pathogenesis of ischaemic, and congenital heart disease has been emphasised, most previous studies have been restricted to simple measurements of right ventricular volumes and ejection fraction. Few attempts have been made to apply to

the right ventricle those more sophisticated indices of function that have greatly enhanced our knowledge of the left ventricle, such as data derived from ventricular pressure-volume loops. An animal study⁸ and a radionuclide study in patients with acquired heart disease9 have suggested that there may be fundamental differences between the pressure-volume relations of the normal left and right ventricles; however, the normal right ventricular pressure-volume relation has vet to be defined angiographically. This study was therefore designed to examine the normal right ventricular pressurevolume relation, using Simpson's rule to measure right ventricular volume from biplane right ventriculograms combined with simultaneous high fidelity pressure recordings.

Patients and methods

RIGHT VENTRICULAR VOLUME DETERMINATION

Right ventricular casts

Twenty two radio-opaque casts of animal (ovine, porcine n = 16), and human (n = 6) right ventricles were made with acrylic resin and radiographic contrast material. The hearts were prepared by oversewing both atrioventricular valves, and a purse string suture (placed around each great vessel) was tightened around a large bore cannula through which the resin-contrast mixture was introduced. The right and left ventricles were distended to filling pressures of 10 and 13 cm of resin and contrast mixture (equivalent to approximately 8 and 10 mm Hg respectively) in an attempt to preserve the normal geometry of the interventricular septum. The hardened cast was dissected from the right ventricle and any residual tissue was removed by immersion in concentrated sodium hydroxide. Cast volumes were determined by water displacement and the mean of five separate estimations was taken.

Angiographic volume estimation

Each cast was then placed in its anatomical position on the catheterisation table. Biplane ventriculograms were recorded on 35 mm cinefilm at 50 frames per second in anteroposterior, lateral, and 30° right anterior oblique, 60° left anterior oblique projections. Calibration was made by a modification of the linear shift method, 10 and the magnification factor was calculated from angiograms exposed before and after the cast was moved 10 cm within the x ray field such that:

magnification factor = observed shift/actual shift.

A single frame from each of the orthogonal views was then projected on to a Summagraphics digi-

tising plate interfaced with a Prime 750 computer and the cast outline was traced by hand. No attempt was made to follow precisely the pattern of trabeculae or papillary muscles. Instead a smooth line was traced around the outermost perimeter of the cast silhouette. For each outline approximately 100 x,y coordinates were recorded and stored on magnetic tape for later analysis. Three dimensional reconstructions were plotted from these stored data (fig 1) by a computer program that is described in detail elsewhere. 11 We used Simpson's rule to calculate the volume of the casts. Briefly, the ventricular outline was divided into 40 equal segments along its long axis. The cross sectional area of each segment was assumed to be elliptical and the diameters of the major and minor axes were calculated from each of the angiographic views. Simpson's rule was then applied to calculate the volume of each slice, and the total volume of the ventricle according to the

$$Volume = \frac{\pi h}{3} \left(\sum_{1}^{39} d1_{O} d2_{O} + \frac{1}{2} \sum_{2}^{40} d1_{E} d2_{E} \right),$$

where h = slice depth, d1 and d2 are the major and minor diameters respectively, and O = odd numbered slices, and E = even numbered slices.

PATIENTS

Ten adults (mean age 37 years, range 29-47, six men, four women) were studied. All were undergoing cardiac catheterisation to establish a clear diagnosis for atypical chest pain. No patient had clinical or electrocardiographic evidence of previous myocardial infarction or arrhythmia and no patient was taking regular cardiac medication. The Brompton Hospital Ethical Committee approved the study and all patients gave their informed written consent.

Cardiac catheterisation

Patients were studied without premedication. Routine left ventriculography and coronary angiography were performed from a femoral approach with the patient supine. After the demonstration of normal left heart haemodynamic function, left ventriculography, and coronary arteriography at least 15 minutes were allowed to elapse before right heart catheterisation was performed. All right heart pressures were measured by a micromanometer tipped catheter with a high-flow lumen through which angiography was performed (Millar Instruments Inc). The transducer of this catheter has a linear response with an output accuracy of $\pm 0.5\%$ between -50 and +300 mm Hg and a frequency response from 0 to 20 kHz. Before insertion the transducer was set at zero for the mid-chest level and calibrated to +100 mm Hg with an external cali-

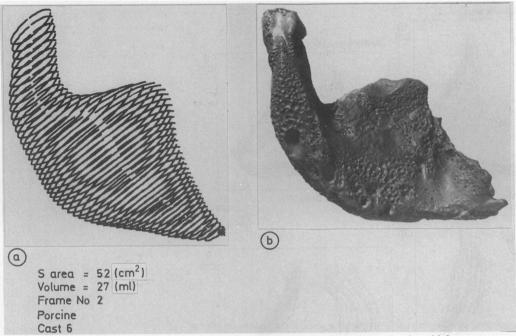


Fig 1 Right ventricular cast and computer-derived three dimensional reconstruction from biplane angiogram.

bration source. We took care to position the catheter tip in the apex of the right ventricle. While the patients held their breath mid-inspiration biplane right ventriculograms recorded anteroposterior and lateral projections on 35 mm film during the injection of 30 ml of radiographic contrast medium (Isopaque). Simultaneous recordings of right ventricular pressure were made at a paper speed of 200 mm/s and an event mark was pressed when contrast material appeared in the right ventricle. To enable exact synchronisation an electrocardiograph timing mark was recorded simultaneously on both cine and pressure recordings. At the end of the study the catheter was left in the right ventricle and the patient was shifted 10 cm in a craniocaudal direction. A cine film was recorded in both projections for later calibration.

ANALYSIS OF ANGIOGRAMS

Each view of the biplane right ventriculogram was digitised with the equipment described above. Only sinus beats were analysed; extrasystoles and post-extrasystoles were discarded. Starting at the R wave of the electrocardiogram successive frames were projected on to the digitising table and cavity outlines were traced frame by frame throughout the cycle. Once again no attempt was made to follow the trabecular pattern precisely. This procedure was

repeated for the same cycle in the orthogonal view and finally the pressure curve recorded during the cycle was digitised by the same equipment, data points being extracted every 20 ms corresponding to each frame of the angiogram. All data were stored on magnetic tape and the following were derived:

- (a) Superimposed plots of cavity outlines throughout the cardiac cycle (fig 2)
- (b) Graphs displaying changes of cavity volume, and pressure throughout the cardiac cycle (fig 3), from which measurements of end diastolic and end systolic volumes were made and corrected for body surface area (ml/m²). Right ventricular ejection fraction was calculated as the ratio of stroke volume to end diastolic volume.
- (c) Pressure-volume loops showing instantaneous changes of pressure and volume throughout the cardiac cycle (figs 4 and 5), and from these loops the following measurements were made: (i) right ventricular ejection before and after peak right ventricular pressure expressed as a percentage of the total stroke volume; (ii) the external mechanical work performed by the right ventricle during systole. This is equivalent to the area enclosed by the pressure volume loop and was determined by automatic planimetry, with systolic stroke work being expressed in J/m^2 body surface area (1 mm Hg.ml = 1.36×10^{-4} J); and (iii) cycle efficiency, which was

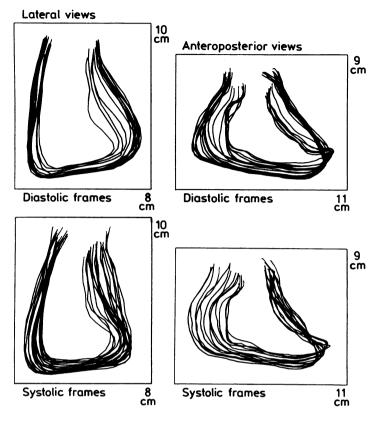


Fig 2 Superimposed plots of cavity outlines from successive frames of each of the biplane views of a right ventriculogram.

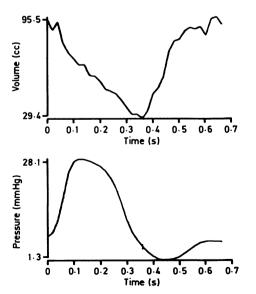


Fig 3 Plots showing simultaneous right ventricular pressure and volume curves.

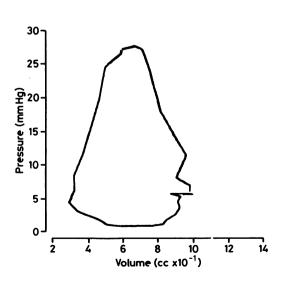


Fig 4 Normal right ventricular pressure-volume loop derived from the curves shown in fig 3.

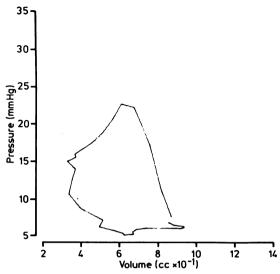


Fig 5 Normal right ventricular pressure-volume loop. In this example there is a better defined limb of isovolumic relaxation. Maximum work 944.8 mm Hg × ml and efficiency 62%.

measured by a method previously described for the left ventricle¹² and expressed as the ratio of the area enclosed by the loop to that of a square or rectangle that just encloses it. This represents the ratio of actual work done to the maximum possible performed by a ventricle with the same stroke volume and pressure change.

In each case the cycle was digitised on another occasion and where possible (n = 7) a second cycle was digitised to assess intraobserver and beat to beat variation.

STATISTICAL ANALYSIS

Group data were expressed as mean (1 SD). The actual cast volumes, measured by fluid displacement, were compared with volumes calculated by linear regression analysis by the method of least squares.

In the clinical studies intraobserver and beat to beat variability of ventricular volumes and ejection fraction were expressed as the mean percentage difference and as a coefficient of repeatability. Assuming that the mean difference between the two sets of observations is zero (that is there is no systematic over or underestimation) and that the difference is unrelated to the absolute size of the measurement (for example the error does not increase with the size of the ventricle), this coefficient is equal to two standard deviations of the mean absolute difference, and is thus expressed in the same units as the original measurements.

Results

CAST DATA

The volume of the casts ranged from 10 to 91 ml. Fig 6a and b shows the relation between cast volume measured by fluid displacement and volume derived from the two pairs of orthogonal views. Excellent correlation coefficients were obtained (both r=0.99), with low standard errors and Y intercepts suggesting that the method was applicable to calculation of small volumes. The regression equations for each pair of orthogonal views were: (i) anteroposterior and lateral views: volume (true) = 0.86 volume (calc) +0.68 (SEE = 4 ml; p < 0.001); (ii) right and left anterior oblique views: volume (true) = 0.81 volume (calc) +0.48 (SEE = 4 ml; p < 0.001).

PATIENT DATA

Left heart haemodynamic function and coronary arteries were normal in all patients. Peak right ventricular systolic pressure was 26 (4) mm Hg, and right ventricular end diastolic pressure was 6 (4) mm Hg. There was no angiographic evidence of tricuspid regurgitation in any of the patients. Satisfactory right ventriculograms were obtained in all, but because of technical problems such as multiple extrasystoles or poor opacification only a single beat was available for analysis in three of the 10 patients. Calculated right ventricular volumes were corrected by the regression equations shown above and expressed per square metre body surface area. End diastolic volume index was 64 (13) ml/m² and stroke volume index was 43 (8) ml/m². The mean right ventricular ejection fraction for the group was 62(6)%.

RIGHT VENTRICULAR PRESSURE-VOLUME RELATIONS

Right ventricular pressure-volume loops tended to be more triangular than the typical left ventricular pressure-volume loop (fig 7). Ejection from the ventricle began early during pressure upstroke with a mean of 39 (4%) of the stroke volume being ejected before peak right ventricular pressure. Consequently there was a poorly defined phase of isovolumic contraction. Interestingly ejection continued well beyond the development of peak right ventricular pressure with 43 (9)% of the stroke volume being ejected during pressure fall. In only five patients was there a well defined end systolic shoulder to the loop (fig 5).

Right ventricular systolic stroke work was $0.078 + 0.021 \text{J/m}^2$ per beat and the resulting cycle efficiency was 56 (8)% (normal for left ventricle = 72-84%).

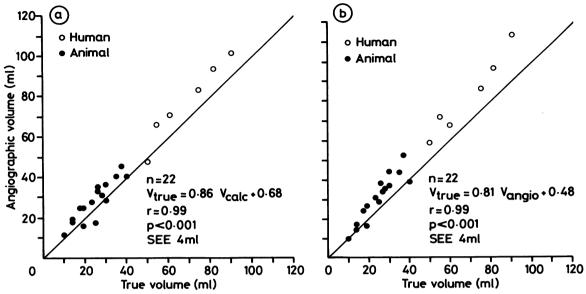


Fig 6 Graphs showing the relation between right ventricular cast volumes measured by fluid displacement and from biplane angiograms. (a) Anteroposterior and lateral views. (b) 30° right anterior oblique and 60° left anterior oblique views.

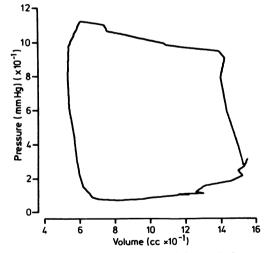


Fig 7 Typical example of a normal left ventricular pressure-volume loop.

INTRAOBSERVER AND BEAT TO BEAT REPRODUCIBILITY

The table shows intraobserver and beat to beat repeatability.

Discussion

Investigation of left ventricular pressure-volume relations has greatly increased our understanding of

Table Intraobserver and beat to beat reproducibility of measured variables

	EDV	SV	RVEF
Intraobserver:			
Mean % difference	5.9	6⋅8	5.9
Coefficient of repeatability	5⋅2	3.6	4.0
Beat to beat $(n = 7)$:			
Mean % difference	11.2	13.5	12.9
Coefficient of repeatability	9.2	9.8	14.0

EDV, end diastolic volume; SV, stroke volume; RVEF, right ventricular ejection fraction.

left ventricular function and it is perhaps surprising, therefore, that there is so little information on right ventricular pressure-volume relations. One explanation is the difficulty of accurately measuring right ventricular volume because of its complex geometry. Nevertheless, several attempts have been made. ^{1 3 5} Although methods based on area-length derivations and geometric models ^{1 - 3} accurately measure the volumes of casts of the right ventricle, they may be inappropriate for the measurement of right ventricular volume throughout the cardiac cycle because changes in cavity shape and spatial orientation during contraction and relaxation, and under the abnormal conditions of chronic pressure or volume overload, make it unlikely that a single geometric model can be applied in all circumstances.

Methods using Simpson's rule go some way towards overcoming these difficulties but certain

geometric assumptions are inherent in any method that attempts to measure ventricular volume from angiograms. In this study we have assumed that each slice of the right ventricle is elliptical and when we digitised both the casts and ventriculograms we included papillary muscles and trabeculae in the cavity outline. It is not surprising, therefore, that our method overestimates ventricular volumes when compared with those derived from fluid displacement of the casts. None the less, this overestimation appears to be consistent and, by applying the appropriate regression equation, right ventricular volume can be estimated with a degree of accuracy approaching that previously described for the left ventricle.14 Indeed simple measurements of end diastolic and end systolic volumes in our patients were similar to those reported by others⁵ 15 and the derived stroke volume index (43 (8) ml/m²) is similar to that reported for the left ventricle. 16 Thus it should be possible to apply our technique to frame by frame analysis of right ventricular volume in a manner similar to that previously performed for the left ventricle.

Gated blood pool radionuclide angiography has been used to assess right ventricular pressurevolume relations⁹ but such techniques calculate volume changes by averaging data obtained from many cardiac cycles and hence pressure and volume measurements can never be truly simultaneous. Furthermore, the relatively low sampling rate (30 frames per second) and variations in the RR interval during data acquisition introduce additional errors. In our study right ventricular volume was calculated every 20 ms and close synchronisation of pressure and volume was achieved. Beat to beat variability and intraobserver variability of measured indices were acceptable and the overall shape of the right ventricular pressure-volume loops was both reproducible and similar in all patients.

The very different loading conditions of the right and left ventricles might be expected to influence their relative pressure-volume characteristics and indeed this has been suggested by the study of crosscirculated canine right ventricles.8 The authors of this report commented on the triangular shape of the right ventricular pressure-volume loop resulting from the continued fall in cavity volume after peak right ventricular pressure. Our study confirms these findings in human beings. Unlike the square or rectangular loop of the normal left ventricle (fig 7) in which there is little change in cavity volume during the two isovolumic periods and in which there is a well defined end systolic shoulder, we have shown that ejection from the right ventricle began during the pressure upstroke and consequently a phase of isovolumic contraction was difficult to define. The observation that ejection continued while right ventricular pressure was falling was a striking feature in our study; as much as 60% of the stroke volume was ejected after peak systolic pressure. In only five patients was there a well-defined end systolic shoulder to the pressure-volume loop.

That the right ventricle can continue to eject during a fall in pressure was suggested indirectly from observations by Shaver et al in 1974 who, using simultaneous right ventricular and pulmonary artery pressure measurements, described a so-called "hangout period" of up to 90 ms between right ventricular pressure fall and pulmonary valve closure in patients with normal right heart pressures. 17 The ability of the right ventricle to eject blood as cavity pressure is falling presumably reflects the low hydraulic impedance to flow and high capacitance of the normal pulmonary vascular bed since this hangout period was greatly reduced when pulmonary vascular resistance was raised. There are no human right ventricular pressure-volume data on the effect of pressure loading, but further support for this phenomenon being a load-dependent one, rather than an intrinsic property of the right ventricular myocardium, comes from similar appearances pressure-volume loops obtained from left ventricles ejecting against the much reduced afterloads that are present after the Mustard operation (unpublished observations) and during treatment with vasodilators.18

The external mechanical work performed by the right ventricle on the circulation during systole is equal to the area enclosed by the pressure-volume loop. 19 The ratio of this area to the area of a square or rectangle that just encloses it represents the ratio of actual work done to the maximum possible done by a ventricle with the same pressure and volume changes and has been termed "cycle efficiency". Despite the finding that the work performed by the right ventricle in ejecting its stroke volume is considerably lower than that for the left ventricle, its "efficiency", as measured by this index, is low (58 (6)%). Cycle efficiency is, however, simply a measure of the ability of the ventricle to act as a square wave pump and the low cycle efficiency observed for the normal right ventricle should not be interpreted as a reflection of efficiency in terms of its energetics, but rather as a convenient method of quantifying the departure of the shape of its pressure-volume loop from that of a square or rectangle.

Indeed there is evidence that the right ventricle may be more efficient than the left in terms of its energetics. It has been demonstrated previously that a considerable amount of potential energy stored in the left ventricular wall at end systole is dissipated in isovolumic relaxation.²⁰ In experimental prepara-

tions much of this potential energy can be converted to external mechanical work by manipulating the afterload against which the left ventricle ejects. Left ventricular pressure-volume loops under these circumstances are similar in shape to those we have recorded for the normal right ventricle and this suggests that the normal right ventricle may be converting more of the potential energy stored in its walls at maximum pressure into external mechanical work.

Further studies are required to evaluate the effect of loading conditions on the human right ventricular pressure-volume relation and until then the clinical implications of our results are likely to be speculative. Our observations do suggest, however, that previous measurements of isovolumic and end systolic indices of right ventricular contractility should be interpreted with caution.

We have shown that it is possible to measure right ventricular volume throughout the cardiac cycle and construct pressure-volume loops. Analysis of these loops showed fundamental differences between the pressure-volume relation of the normal left and right ventricles, which presumably reflect the low hydraulic impedance to flow in the pulmonary circulation.

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